

Comprehensive Guide to Transformer Zero-Sequence Impedance: Engineering Theory, Measurement, and Calculation

Published: September 9, 2026 | Index ID: #655

In the domain of electrical power systems engineering, understanding the behavior of three-phase transformers under unbalanced fault conditions is paramount for ensuring system stability and protection. Central to this understanding is the concept of **zero-sequence impedance (Z0)**. Unlike positive and negative sequence impedances, which are generally equal in static equipment like transformers, the zero-sequence impedance is highly dependent on the magnetic circuit's construction, winding connections, and even the presence of a tank. This technical analysis explores the theoretical framework, measurement methodologies, and calculation techniques required for a deep understanding of zero-sequence impedance in power transformers.

Fundamental Concepts of Zero-Sequence Impedance

Zero-sequence impedance is defined as the impedance offered by a network to the flow of zero-sequence currents. In a three-phase system, zero-sequence currents are three currents that are equal in magnitude and in phase with one another. For these currents to flow in a transformer, there must be a physical path to a neutral or ground point.

The significance of **zero-sequence impedance** becomes critical during Single Line-to-Ground (SLG) and Double Line-to-Ground (DLG) faults. The magnitude of the fault current is inversely proportional to the sum of the positive, negative, and zero-sequence impedances of the system. In many configurations, the transformer's zero-sequence impedance is the dominant factor limiting ground fault current. Consequently, accurate determination of this value is essential for the sizing of neutral grounding resistors (NGRs), the setting of overcurrent and ground fault relays, and the design of insulation systems.

The Role of Symmetrical Components

According to Fortescue's Theorem, any unbalanced three-phase system can be decomposed into three balanced systems of phasors: positive sequence (rotating in the normal order), negative sequence (rotating in reverse order), and zero sequence (non-rotating, in-phase). In a transformer, the **positive-sequence impedance (Z1)** and **negative-sequence impedance (Z2)** are essentially the leakage impedance measured during a standard short-circuit test. However, **Z0** behaves differently because the magnetic flux produced by in-phase currents does not sum to zero in the core as it does with balanced currents.

Influence of Core Construction on Zero-Sequence Impedance

One of the most complex aspects of zero-sequence impedance is its dependence on the mechanical and magnetic architecture of the transformer core. The path that the magnetic flux must take when zero-sequence currents are applied determines the magnitude of the impedance.

1. Three-Limb Core Transformers

In a **three-limb core**, there is no physical fourth or fifth limb to provide a return path for the in-phase zero-sequence flux. Consequently, the flux is forced to exit the core and return through the air, the transformer oil, and the steel tank. Because the reluctance of air and oil is significantly higher than that of grain-oriented electrical steel,

the magnetizing zero-sequence impedance is much lower than the positive-sequence magnetizing impedance. However, the tank acts like a high-resistance short-circuited winding, which significantly influences the final measured value of Z_0 .

2. Five-Limb and Shell-Type Cores

In **five-limb cores** or **shell-type transformers**, dedicated return paths for the flux exist within the core structure itself. In these designs, the zero-sequence flux can remain entirely within the high-permeability steel. As a result, the zero-sequence magnetizing impedance is very high, often approaching the positive-sequence magnetizing impedance. In these cases, Z_0 is typically considered equal to the positive-sequence leakage impedance (Z_1) if a delta winding is present to circulate the current.

The Impact of Winding Connections

The vector group and winding connection of a transformer dictate whether zero-sequence current can even exist within a specific winding. The following table summarizes the behavior of Z_0 based on common connections:

Winding Connection	Z0 Characteristic	Path for Zero-Sequence Current
Wye-Grounded (Yn)	Dependent on secondary	Permits flow to neutral; depends on the magnetic circuit.
Delta (D)	Infinite (Open Circuit)	Zero-sequence currents can circulate within the delta but cannot enter or exit the lines.
Wye (Y - Ungrounded)	Infinite	No return path for zero-sequence current exists.
Yn-d (Grounded Wye-Delta)	Low Impedance	The delta winding acts as a short circuit for zero-sequence flux, creating low Z0.

The YNynd Connection (Part 01 Analysis)

A specific case mentioned in technical studies is the **YNynd** configuration (Star with neutral, Star with neutral, and an internal Delta). In this configuration, the Delta winding serves as a tertiary winding. Its primary purpose regarding zero-sequence impedance is to provide a low-impedance path for zero-sequence currents, thereby stabilizing the neutral point and limiting the zero-sequence voltage shift during faults. When calculating Z0 for such a transformer, engineers must account for the parallel combination of the magnetic path and the tertiary winding's leakage impedance.

Measurement Procedures for Zero-Sequence Impedance

Field testing is the most reliable method for determining the actual zero-sequence impedance of a transformer, especially for older units where documentation may be missing or for 3-limb units where tank effects are unpredictable.

Test Setup and Workflow

To measure the zero-sequence impedance of a specific winding (usually the high-voltage or low-voltage star-connected winding), the following steps are executed:

1. Isolate the Transformer: Ensure the transformer is disconnected from the power grid and properly grounded for safety.
2. Connect Terminals in Parallel: Short the three phase terminals (H1, H2, H3 or X1, X2, X3) together.
3. Apply Single-Phase Voltage: Apply a single-phase AC voltage source between the joined terminals and the neutral terminal.
4. Secondary Side Configuration: Depending on the test objective, the secondary winding may be left open or short-circuited. For Z0 measurement used in fault studies, the secondary is typically left in its normal operating state (e.g., if it's a Delta, it remains closed).
5. Measure Voltage and Current: Record the applied voltage (V) and the total current (I) flowing into the three phases.

The formula to calculate the zero-sequence impedance per phase is:

$$Z_0 = 3 * (V / I)$$

The factor of 3 arises because the three phase-windings are connected in parallel, meaning the applied voltage

drives current through all three simultaneously. The resulting value is typically expressed in ohms per phase and then converted to a percentage or per-unit (pu) value based on the transformer's rating.

Measurement Constraints

When performing these tests, it is crucial to keep the current level below the rated phase current to prevent overheating. However, for 3-limb transformers, the current must be high enough (usually 10% to 30% of rated) to ensure that the flux penetrates the tank and provides a realistic representation of fault-level impedance.

Calculating Zero-Sequence Impedance Using Numerical Methods

While measurement is ideal for existing units, **Finite Element Analysis (FEA)** and numerical methods are employed during the design phase. Calculating the Z0 of 3-limb transformers is notoriously difficult because the return path for the flux involves non-linear magnetic materials (the tank) and complex air gaps.

Rules to Estimate Expected Values

Engineering rules of thumb provide a baseline for expected Z0 values in 3-limb core transformers:

- Without a Delta Winding: Z0 is typically 30% to 100% of the magnetizing impedance, but significantly higher than the positive-sequence leakage impedance.
- With a Delta Winding: Z0 is roughly equal to the positive-sequence leakage impedance (Z0 "H 0.8 to 1.0 times Z1).
- Underground Cables: For transformers connected to underground cables, the zero-sequence impedance of the cable itself must be calculated using the Method of Images or Carson's equations to account for the earth return path and sheath currents.

Technical Comparison: 3-Limb vs. 5-Limb Behavior

The following table illustrates the key technical differences between core designs when subjected to zero-sequence excitation.

Feature	3-Limb Core	5-Limb Core	Shell-Type
Zero-Sequence Flux Path	Through air and tank	Through outer core limbs	Through core laminations
Z0 Magnitude (No Delta)	Medium (due to tank losses)	Very High	Very High
Tank Heating Risk	High during sustained faults	Negligible	Negligible
Reluctance	High	Low	Low

Practical Implementation and Field Considerations

When integrating transformer zero-sequence data into a **Short-Circuit Current Calculation**(such as those performed via Eaton or ETAP software), engineers must ensure that the sequence networks are connected correctly. For a Ynd transformer, the zero-sequence network is a series impedance connected to the ground at the Wye side, while the Delta side remains an open circuit in the zero-sequence diagram.

Case Study: Tank Overheating in 3-Limb Transformers

In a real-world scenario involving a 100MVA 3-limb transformer without a tertiary delta winding, a sustained unbalanced load led to significant overheating of the transformer tank. Technical investigation revealed that the zero-sequence flux, unable to return through the core, induced massive eddy currents in the steel tank. This serves as a critical reminder: **Z0 is not just a calculation parameter but a physical phenomenon with thermal implications.** Designers must often include "tank shields" (aluminum or copper plates) to provide a low-resistance path for these eddy currents and prevent localized hotspots.

Troubleshooting and Common Errors

Discrepancies between calculated and measured Z0 values often stem from:

- Ignoring the Tank: Failing to account for the tank as a parallel conductive path.
- Saturation Effects: Measuring Z0 at very low voltages where the core iron is not yet in its linear operating region.
- Tertiary Winding Omissions: Forgetting that even an unloaded delta tertiary winding significantly reduces Z0.

Advanced Estimation for Power Transformers

Modern power systems utilize high-speed protection that requires precise Z0 values. If a measurement is impossible, the **Standard Reactance Method** can be used. This involves taking the positive-sequence reactance (X1) and applying a multiplier based on the core type and the presence of a stabilizing winding. For a standard 3-limb YNyn transformer, a common multiplier for Z0 is 0.85 times the magnetizing reactance, though this is a broad approximation and should be verified against manufacturer test reports whenever possible.

The zero-sequence impedance of a transformer is a multidimensional parameter influenced by electromagnetic theory, mechanical design, and circuit topology. While positive and negative sequence impedances remain relatively stable across different core types, Z0 requires a nuanced approach that considers flux return paths and the conductive properties of the transformer tank. By combining rigorous measurement techniques with advanced numerical calculations and historical estimation rules, electrical engineers can accurately predict system behavior during ground faults, ensuring the safety and reliability of the power grid. As systems evolve with more renewable

integration and varied grounding practices, the mastery of zero-sequence dynamics remains a cornerstone of professional electrical engineering practice.

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